

DESCRIPTION

PD_MC).

details).

DC converters and motor drive.

XTR25010 is a high-temperature, high reliability power transistor driver integrated circuit designed to drive normally ON and normally-OFF power transistors in Silicon Carbide (SiC), Gallium Nitride (GaN) and standard silicon, including JFETs, MOSFETs, BJTs, SJTs and MESFETs. For turning on the power transistors, the XTR25010 includes two independent pull-up gate-drive-channels (PU_DR1 and PU_DR2) capable of sourcing 4A at 230°C peak current each. For turning off the power transistors, the XTR25010 includes two pull-down gate-drivechannels capable of sinking 3A at 230°C peak current each (PD_DR and

For driving wide bandgap transistors, it is recommended to use XTR25010 as a power stage extension for the XTR26010, which generates the needed control signals and additional protection functions (see XTR26010 datasheet and application note for more

XTR25010 can also be used standalone as a half-bridge driver for DC-

FEATURES

- Operational beyond the -60°C to +230°C temperature range.
- High voltage supply from 7V to 35V.
- Low voltage supply from 4.5V to 5.5V
- Integrated charge-pump inside pull-up drivers allowing 100% dutycycle PWM control signal.
- Double pull-up drivers with combined 8A peak and 2A continuous current capability at $T_c = 230^{\circ}$ C.
- Two pull-down drivers with 3A peak current capability at $T_c = 230^{\circ}$ C for each driver.
- Nonoverlapped pull-up and pull-down outputs.
- Enable input signal for driver outputs reset.
- Latch-up free.
- Ruggedized SMT packages and also available as bare die.

APPLICATIONS

• Reliability-critical, Automotive, Aeronautics & Aerospace, Downhole.

- Intelligent Power Modules (IPM).
- Power inverters.
- Power conversion and motor drive.
- DC-DC converters and switched mode power supplies.

PRODUCT HIGHLIGHT

Other packages and packaging configurations possible upon request. For some packages or packaging configurations, MOQ may apply.

TYPICAL APPLICATIONS

Power Transistor Driver

ABSOLUTE MAXIMUM RATINGS

Caution: Stresses beyond those listed in "ABSOLUTE MAXIMUM RATINGS" may cause permanent damage to the device. These are stress ratings only and functionality of the device at these or any other condition beyond those indicated in the operational sections of the specifications is not implied. Exposure to "ABSOLUTE MAXIMUM RATINGS" conditions for extended periods may permanently affect device reliability.

PACKAGING

Die level block diagram showing all available functionalities and bond-pads. Arrows aside pad names indicate whether the input is internally pulled up or down by default (with about 100kΩ strength).

PIN DESCRIPTION

¹ *PVSS and VSS are internally connected through two anti-parallel diodes. PVSS and VSS shall be connected to the same voltage through a star-like connection.*

THERMAL CHARACTERISTICS

RECOMMENDED OPERATING CONDITIONS

¹ For gate drive application, it is recommended to add two decoupling capacitors in the range of 100nF to 1µF, one between VCC and SOURCE terminal of the power transistor and the other between VSS and SOURCE terminal of the power transistor. These capacitors must be placed close to the power *transistor to minimize the transient gate current paths for EMI reduction.*

² Add a decoupling capacitor in the range of 100nF to 1µF between VDD and VSS supply planes as close as possible to pins VDD and PVDD.

³ Operation beyond the specified temperature range is achieved

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ESD CLAMPING SCHEME

ELECTRICAL SPECIFICATIONS

Unless otherwise stated, specification applies for VDD-VSS=5V, VCC-VSS=25V (PVCC_DR1 and PVCC_DR2 connected to VCC) and -60°C≤Tc≤230°C. Typical values are given at Tc=25°C.

¹ The rise/fall time measurement strongly depends on parasitic capacitance at the output of the driver. This measurement has been performed with all *driver outputs shorted (PU_DRx, PD_DR_x, PD_MC_x), which adds a significant parasitic capacitance (estimated to 400pF) to the 1nF capacitance connected at the output.*

TYPICAL PERFORMANCE

Figure 1. Quiescent current consumption on VDD versus temperature (EN=IN_SSD=1, IN_DR1=IN_DR2=IN_PD=IN_MC=0, VCC=25V).

Figure 3. Dynamic current consumption on VDD versus frequency for several case temperatures (C_{LOAD}=1nF, V_{CC}=25V, V_{DD}=5V).¹

Figure 5. R_{ON} of pull-down driver (DR_PD) versus case temperature for several V_{DD} (ILOAD=200mA, Vcc=25V).

Figure 2. Quiescent current consumption on VCC versus temperature (EN=IN_SSD=1, IN_DR1=IN_DR2=IN_PD=IN_MC=0).

Figure 4. Dynamic current consumption on VCC versus frequency for several case temperatures (C_{LOAD}=1nF, V_{CC}=25V, V_{DD}=5V).

Figure 6. R_{ON} of Miller Clamp driver (DR_MC) versus case temperature for several V_{DD} (ILOAD=200mA, Vcc=25V).

¹ The dynamic current consumption on VDD supply significantly increases below 1kHz PWM frequency due to charge pump turn-on.

TYPICAL PERFORMANCE (CONTINUED)

Figure 9. Ron of pull-up driver (DR2_PU) versus case temperature for several V_{DD} (I_{LOAD}=200mA, Vcc=25V).

Figure 11. V_{DS} versus continuous output current of pull-up driver (DR2_PU) for different V_{DD} (Tc=230°C, Vcc=25V).

Figure 10. V_{DS} versus continuous output current of pull-up driver (DR1_PU) for different V_{DD} (Tc=230°C, Vcc=25V)

Figure 12. Peak output current of pull-down driver (DR_PD) versus case temperature for several V_{DD} (C_{LOAD}=100nF, Vcc=25V).

TYPICAL PERFORMANCE (CONTINUED)

Figure 13. Peak output current of Miller Clamp driver (DR_MC) versus case temperature for several V_{DD} (C_{LOAD}=100nF, Vcc=25V)

Figure 15. Peak output current of pull-up driver (DR_PU2) versus case temperature for several V_{DD} (V_{CC}=25V)

Figure 17. Propagation delay from IN_DR2 to PU_DR2 versus case temperature for several V_{CC} (C_{LOAD}=1nF, V_{DD}=5V).

Figure 14. Peak output current of pull-up driver (DR_PD1) versus case temperature for several V_{DD} (C_{LOAD}=100nF, Vcc=25V).

Figure 16. Propagation delay from IN_DR1 to PU_DR1 versus case temperature for several Vcc (CLOAD=1nF, VDD=5V)

Figure 18. Propagation delay from IN_DR1 to PD_DR versus case temperature for several V_{cc} (C_{LOAD}=1nF, V_{DD}=5V).

TYPICAL PERFORMANCE (CONTINUED)

Figure 21. Fall time of PD_MC output versus case temperature for several V_{CC} (V_{DD} =5V).

Figure 23. Rise time of PU_DR2 output versus case temperature for several V_{CC} (V_{DD} =5V).

Figure 22. Rise time of PU_DR1 output versus case temperature for several V_{CC} (V_{DD} =5V).

Figure 24. Oscilloscope snap shot showing operation at 1MHz input frequency versus case temperature (PU_DR1, PU_DR2, PD_DR, PD_MC connected, CLOAD=1nF, VDD=5V, Vcc=25V).

THEORY OF OPERATION

Introduction

XTR25010 is a high-temperature, high reliability power transistor driver and controller integrated circuit specifically designed to drive wide bandgap (WBG) power transistors, such as Silicon Carbide (SiC) as well as Gallium Nitride (GaN) transistors including normally-On and normally-Off JFETs, MOSFETs, SJTs, BJTs and HEMTs. For the turn-on of power transistors, the XTR25010 includes two independent pull-up gate-drivechannels (PU_DR1 and PU_DR2) each capable of sourcing 4A at T_c =230°C. For the turn-off of power transistors, the XTR25010 includes two pulldown gate-drive-channels (PD_DR and PD_MC) each capable of sinking 3A peak current at $T_C=230^{\circ}$ C. The PD_DR channel is used for the effective turn-off, while PD_MC channel is used for Active Miller Clamping (AMC).

For driving wide bandgap transistors, it is recommended to use XTR25010 as a power stage extension for the XTR26010, which generates the needed control signals and additional protection functions (see XTR26010 for more details).

For DC/DC converters and motor drive, the XTR25010 can be driven directly with suitable signals from PWM controllers such as XTR30010.

Truth table

- The EN input is master over all other inputs.
- IN SSD is active low.
- The outputs can be set to high impedance with a logic 1 on EN and IN SSD, and logic 0 on all other inputs.

Bootstrap capacitors

The bootstrap capacitor value can be selected taking into account conditions 1, 2 and 3 described hereafter.

Figure 25. Bootstrap capacitor charging (shown in blue) and discharging (shown in red) curves.

The bootstrap capacitor C_{BST} is charged for the first time during the startup time given by the rise time of the power supply. It is recommended to wait for at least a 50µs, after power supply startup, before sending any PWM signal to ensure correct first charge of the CBST. The charging path is, as described in Figure 26 with the blue arrows, going from the 5V versus VSS power supply PVDD via the integrated bootstrap diode, then the external R_{PU}, and finally the PD_MC driver in parallel with the R_{PD} and the PD_DR driver. Hence, C_{BST} must fulfill the following condition to guarantee its total charge during the startup, which gives an upper limit:

As the on resistances of the PU, PD, MC transistors are in the range of 1...2 Ω , they are neglected compared to R_{PU} and R_{PD}. As an example, for R_{PU} =20 Ω , C_{BST} must be smaller than 833nF.

The bootstrap capacitor C_{BST} is discharged into the PU_DR driver during the ON time tow as shown by the red arrows in Figure 26.

As shown in Figure 25, in steady state, the voltage decreases ΔV_{BST} on C_{BST} during discharge (red curve, ON time t_{ON}) is given by:

ΔV_{BST} =(Iq^{*}t_{ON}+C_{eq}*V_{MAX})/C_{BST}

Where $I_Q = 250\mu A$ is the quiescent current delivered from BST_DRx_P to the pull-up driver, Ceq≈500pF is the equivalent capacitor that must be charged by BST_DRx_P up to the voltage V_{MAX} , $t_{ON}=(1/f_R)-t_{OFF}$, and fr is the PWM frequency.

Figure 26. Bootstrap capacitor charging and discharging paths.

To have a first guess for minimum value of CBST, we consider the extreme values for $V_{MAX}=V_{DD}-V_{TD}$ (V_{TD}~0.7V is the forward voltage of the bootstrap diode), and $\Delta V_{\rm BST}=500$ mV to ensure V_{MIN} > 3.75V, which is the threshold to turn-on the integrated charge pump. Indeed, the integrated charge pump has been designed to be able to maintain the on state permanently (PWM DTC 100%). However, the charge pump is not able to provide enough charge to the bootstrap capacitor when the PWM signal is switching. Therefore, the following condition on CBST, which gives a lower limit, is obtained:

Cond. 2: CBST>[Iq*ton+Ceq*(VDD-VTD)]/ ΔV_{BST}

For $V_{DD}-V_{TD}=4.3V$, $f_R=50kHz$, $t_{ON}=19\mu s$ ($t_{OFF}=1\mu s$), and ΔV_{BST} =500mV, C_{BST} must be higher than 13.8nF. As this is an extreme value, we recommend taking at least three times this value to reduce the voltage ripple ΔV_{BST} .

In steady state, as shown in Figure 25, the voltage difference ΔV_{BST} on C_{BST} during the charge period (blue curve, OFF time toff) is given by:

ΔVBST=(VDD-VTD-VMIN)*(1-exp[-tOFF/(Req*CBST)])

Where Req is the total resistance in the charge path of the bootstrap capacitor. When the XTR25010 is used together with XTR26010 for gate drive applications, R_{eq} is given by:

 R_{eq}^{-1} = (R_{PU}+R_{PD})^{-1*}t_{MC}/t_{OFF}+R_{PU}-1* (t_{OFF}-t_{MC})/t_{OFF}

Where t_{MC} is the Miller Clamp delay.

From the equation of ΔV_{BST} during the charge, and considering a given Req, the following condition on CBST is obtained:

Cond. 3: CBST<-toff/(Req*ln[1-ΔVBST/(VDD-VTD-VMIN)])

For V_{MIN}=4V, ΔV_{BST} =150mV, t_{MC}=100ns, torr=1µs, and Req=21 Ω $(R_{PU}=R_{PD}=20\Omega)$, C_{BST} must be smaller than 68.5nF.

With CBST=47nF, $Req=21\Omega$, fr=50kHz, torr=1µs, the following ripple characteristics are obtained:

 $\Delta V_{\text{BST}} = 146$ mV, $V_{\text{MAX}} = 4.21$ V, $V_{\text{MIN}} = 4.07$ V

Application considerations

Forcing a voltage V_{BST} above 6V across the bootstrap capacitor could damage the part. Indeed, during the normal switched operation, as shown in Figure 27, a parasitic charge pump effect can be created that tends to increase the voltage across the bootstrap capacitor. When the PU_DRx driver is on, the internal charge pump capacitor C_{CP} (\sim 100pF) is charged to PVCC voltage following the charge path shown by the blue arrows in Figure 27. Then, when the PD_DR driver is on, C_{BST} is charged via C_{CP} following the charge path shown by the red arrows in Figure 27.

Figure 27. Parasitic charge pump charging (blue arrows) and discharging (red arrows) paths.

To remove the extra charge due to this parasitic charge pump effect, the $XTR25010$ has an internal protection that monitors V_{BST} and enables a discharge path from the bootstrap capacitor top plate (BST_DRx_P) to VSS if V_{BST} exceeds 6V. This discharge path is made of an internal resistor of about $10k\Omega$ connected between BST_DRx_P and VSS. This protection is blanked for 2µs after each PWM rising/falling edge to avoid any spurious activation due to switching noise. Hence, considering a margin of 3µs, for to or to F above 5 us no additional external protection is needed.

For supply voltages (VCC-VSS) above 10V, if the PWM frequency is around or higher than 100kHz and tow or tors are below 5µs, it is recommended to add a 6V clamping diode to avoid damaging the part.

If one of the pull-up drivers DR1_PU/DR2_PU is not used, the corresponding output PU_DR1/PU_DR2 shall be connected to PVSS. Otherwise the unused driver could be damaged due to an excessive charge of the bootstrap capacitor caused by the parasitic charge pump effect.

PACKAGE OUTLINES

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