

## ICL7135C, TLC7135C

### Advanced LinCMOS™ 4 1/2-DIGIT PRECISION ANALOG-TO-DIGITAL CONVERTERS

D2851, DECEMBER 1986—REVISED MARCH 1988

- Advanced LinCMOS™ Technology
- Zero Reading for 0-V Input
- Precision Null Detection with True Polarity at Zero
- 1-pA Typical Input Current
- True Differential Input
- Multiplexed Binary-Coded-Decimal Output
- Low Rollover Error:  $\pm 1$  Count Maximum
- Control Signals Allow Interfacing with UARTs or Microprocessors
- Autoranging Capability with Over- and Under-Range Signals
- TTL-Compatible Outputs
- Direct Replacement for Teledyne TSC7135, Intersil ICL7135, Maxim ICL7135, and Siliconix SI7135

#### description

The ICL7135C and TLC7135C converters are manufactured with Texas Instruments highly efficient Advanced LinCMOS™ technology. This 4 1/2-digit dual-slope-integrating analog-to-digital converter is designed to provide interfaces to both a microprocessor and a visual display. The digit-drive outputs D1 through D4 and multiplexed binary-coded-decimal outputs, B1 through B4, provide an interface for LED or LCD decoder/drivers as well as microprocessors.

The ICL7135C and TLC7135C offer 50-ppm (one part in 20,000) resolution with a maximum linearity error of one count. The zero error is less than  $10 \mu\text{V}$  and zero drift is less than  $0.5 \mu\text{V}/^\circ\text{C}$ . Source-impedance errors are minimized by low input current (less than 10 pA). Rollover error is limited to  $\pm 1$  count.

The BUSY, STROBE, RUN/HOLD, OVER-RANGE, and UNDER-RANGE control signals support microprocessor-based measurement systems. The control signals also can support remote data acquisition systems with data transfer via universal asynchronous receiver transmitters (UARTs).

The ICL7135C and TLC7135C are characterized for operation from  $0^\circ\text{C}$  to  $70^\circ\text{C}$ .



Caution. This device has limited built-in gate protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage.

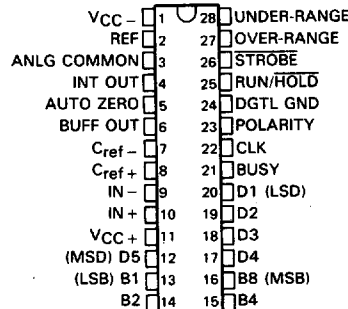
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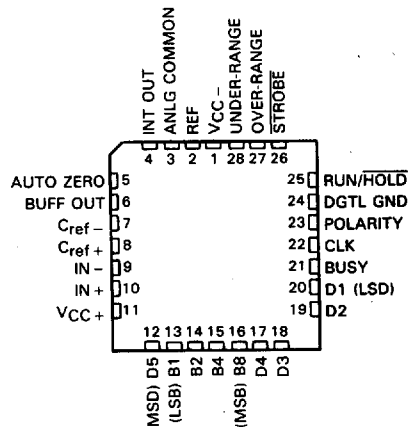
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N PACKAGE  
(TOP VIEW)



FN PACKAGE  
(TOP VIEW)



#### AVAILABLE OPTIONS†

SYMBOLIZATION		OPERATING
DEVICE	PACKAGE SUFFIX	TEMPERATURE RANGE
ICL7135C	FN, N	$0^\circ\text{C}$ to $70^\circ\text{C}$
TLC7135C	FN, N	$0^\circ\text{C}$ to $70^\circ\text{C}$

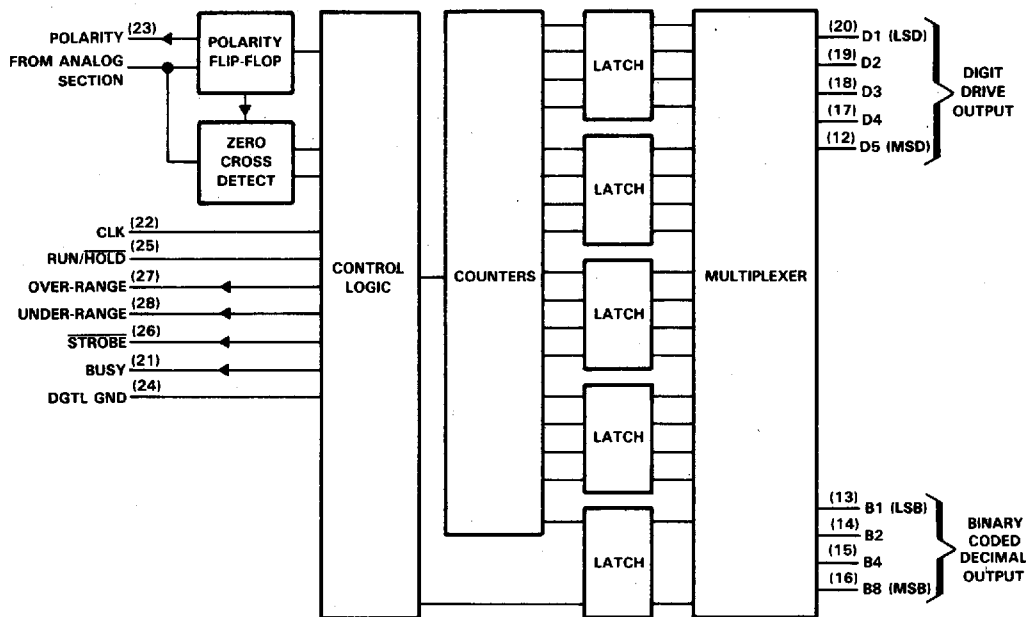
†In many instances, these ICs may have ICL7135C and TLC7135C symbolization on the package.

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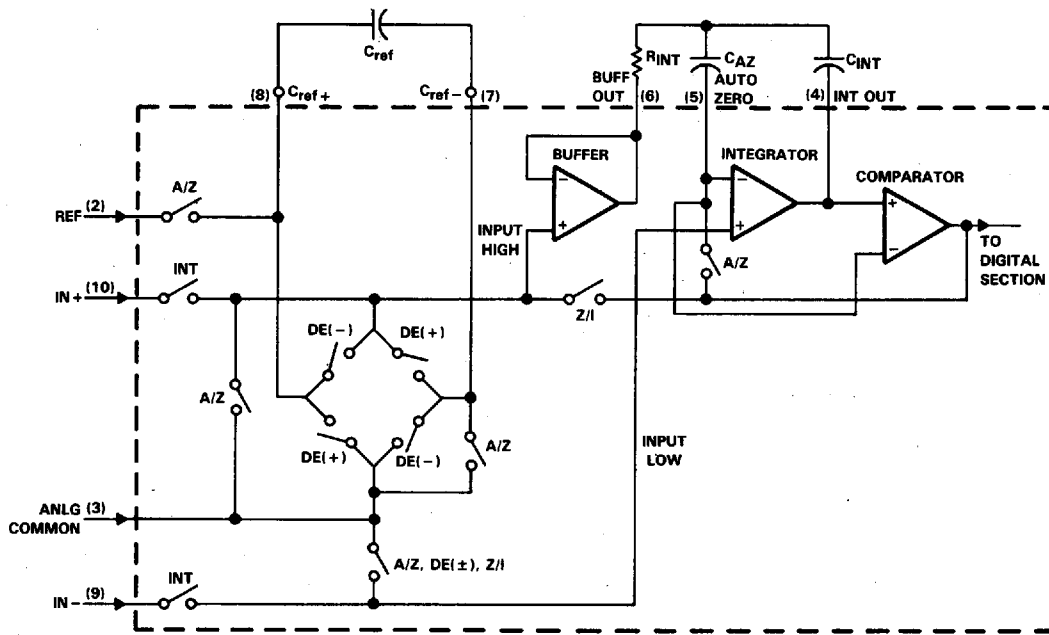
**ICL7135C, TLC7135C**  
**Advanced LinCMOS™ 4 1/2-DIGIT PRECISION**  
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T-51-10-05

functional block diagram



ANALOG SECTION



**ICL7135C, TLC7135C**  
**Advanced LinCMOS™ 4 1/2-DIGIT PRECISION**  
**ANALOG-TO-DIGITAL CONVERTERS**

**absolute maximum ratings over operating free-air temperature range (unless otherwise noted)**

Supply voltage ( $V_{CC+}$ with respect to $V_{CC-}$ )	15 V
Analog input voltage (pin 9 or pin 10)	$V_{CC-}$ to $V_{CC+}$
Reference voltage range	$V_{CC-}$ to $V_{CC+}$
Clock input voltage range	0 V to $V_{CC+}$
Operating free-air temperature range	0°C to 70°C
Storage temperature range	-65°C to 150°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds: N package	260°C
Case temperature for 10 seconds: FN package	260°C

**recommended operating conditions**

T-51-10-05

	MIN	NOM	MAX	UNIT
Supply voltage, $V_{CC+}$	4	5	6	V
Supply voltage, $V_{CC-}$	-3	-5	-8	V
Reference voltage, $V_{ref}$		1		V
High-level input voltage, CLK, RUN/HOLD, $V_{IH}$	2.8			V
Low-level input voltage, CLK, RUN/HOLD, $V_{IL}$			0.8	V
Differential input voltage, $V_{ID}$	$V_{CC-} + 1$		$V_{CC+} - 0.5$	V
Maximum operating frequency, $f_{clock}$ (see Note 1)	1.2	2		MHz
Operating free-air temperature range, $T_A$	0		70	°C

NOTE 1: Clock frequency range extends down to 0 Hz.

**electrical characteristics,  $V_{CC+} = 5 V$ ,  $V_{CC-} = -5 V$ ,  $V_{ref} = 1 V$ ,  $f_{clock} = 120 kHz$ ,  $T_A = 25°C$  (unless otherwise noted)**

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$V_{OH}$	High-level output voltage	D1-D5, B1, B2, B4, B8 $I_O = -1 mA$	2.4		5	V
		Other outputs $I_O = -10 \mu A$	4.9		5	
$V_{OL}$	Low-level output voltage	$I_O = 1.6 mA$			0.4	V
	Peak-to-peak output noise voltage (see Note 2)	$V_{ID} = 0$ , Full Scale = 2 V		15		$\mu V$
$\alpha_{VO}$	Zero-reading temperature coefficient of output voltage	$V_{ID} = 0$ , 0°C ≤ $T_A$ ≤ 70°C		0.5	2	$\mu V/°C$
$I_{IH}$	High-level input current	$V_I = 5 V$ , 0°C ≤ $T_A$ ≤ 70°C		0.1	10	$\mu A$
$I_{IL}$	Low-level input current	$V_I = 0 V$ , 0°C ≤ $T_A$ ≤ 70°C		-0.02	-0.1	mA
$I_I$	Input leakage current, pins 9 and 10	$V_{ID} = 0$ , $T_A = 25°C$		1	10	pA
		$V_{ID} = 0$ , 0°C ≤ $T_A$ ≤ 70°C			250	
$I_{CC+}$	Positive supply current	$f_{clock} = 0$ , $T_A = 25°C$		1	2	mA
		$f_{clock} = 0$ , 0°C ≤ $T_A$ ≤ 70°C			3	
$I_{CC-}$	Negative supply current	$f_{clock} = 0$ , $T_A = 25°C$		-0.8	-2	mA
		$f_{clock} = 0$ , 0°C ≤ $T_A$ ≤ 70°C			-3	
$C_{pd}$	Power dissipation capacitance	See Note 3		40		pF

NOTES: 2. This is the peak-to-peak value that is not exceeded 95% of the time.  
 3. Factor relating clock-frequency to increase in supply current. At  $V_{CC+} = 5 V$

$$I_{CC+} = I_{CC+}(f_{clock} = 0) + C_{pd} \times 5 V \times f_{clock}$$

  
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**ICL7135C, TLC7135C**  
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**ANALOG-TO-DIGITAL CONVERTERS**

T-51-10-05

operating characteristics,  $V_{CC+} = 5\text{ V}$ ,  $V_{CC-} = -5\text{ V}$ ,  $V_{ref} = 1\text{ V}$ ,  $f_{clock} = 120\text{ kHz}$ ,  
 $T_A = 25^\circ\text{C}$  (unless otherwise noted)

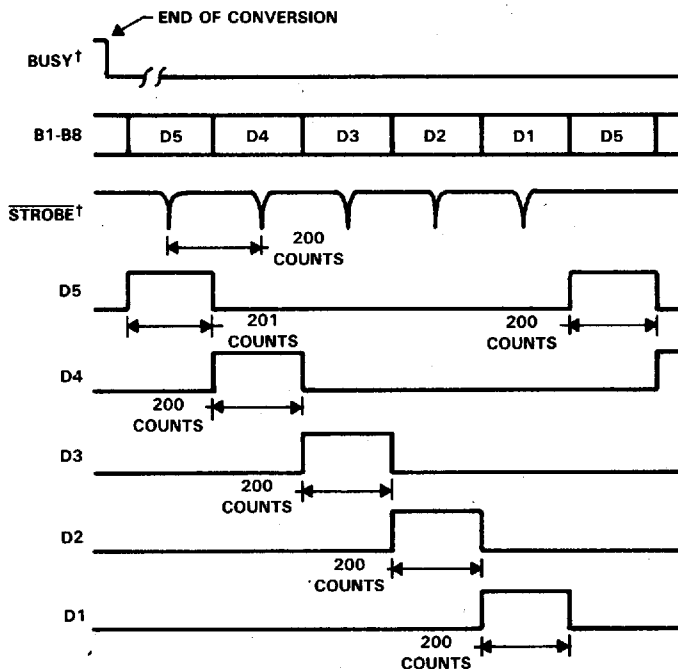
PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
$\alpha_{FS}$ Full-scale temperature coefficient (see Note 4)	$V_{ID} = 2\text{ V}$ , $0^\circ\text{C} \leq T_A \leq 70^\circ\text{C}$			5	ppm/°C
Linearity error	$-2\text{ V} \leq V_{ID} \leq 2\text{ V}$		0.5	1	count
Differential linearity error (see Note 5)	$-2\text{ V} \leq V_{ID} \leq 2\text{ V}$		0.01		LSB
$\pm$ Full-scale symmetry error (see Note 6) (rollover error)	$V_{ID} = \pm 2\text{ V}$		0.5	1	count
Display reading with 0-V input	$V_{ID} = 0$ , $0^\circ\text{C} \leq T_A \leq 70^\circ\text{C}$	-0.0000	$\pm 0.0000$	+0.0000	Digital Reading
Display reading in ratiometric operation	$V_{ID} = V_{ref}$ , $T_A = 25^\circ\text{C}$	+0.9998	+0.9999	+1.0000	Digital Reading
	$0^\circ\text{C} \leq T_A \leq 70^\circ\text{C}$	+0.9995	+0.9999	+1.0005	Digital Reading

- NOTES: 4. This parameter is measured with an external reference having a temperature coefficient of less than 0.01 ppm/°C.  
 5. The magnitude of the difference between the worst case step of adjacent counts and the ideal step.  
 6. Rollover error is the difference between the absolute values of the conversion for 2 V and -2 V.

**ICL7135C, TLC7135C**  
**Advanced LinCMOS™ 4 1/2-DIGIT PRECISION**  
**ANALOG-TO-DIGITAL CONVERTERS**

timing diagrams

T-51-10-05



† Delay between BUSY going low and the first STROBE pulse is dependent upon the analog input.

FIGURE 1

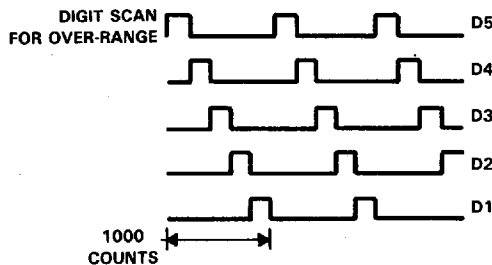


FIGURE 2



**ICL7135C, TLC7135C**  
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T-51-10-05

timing diagrams (continued)

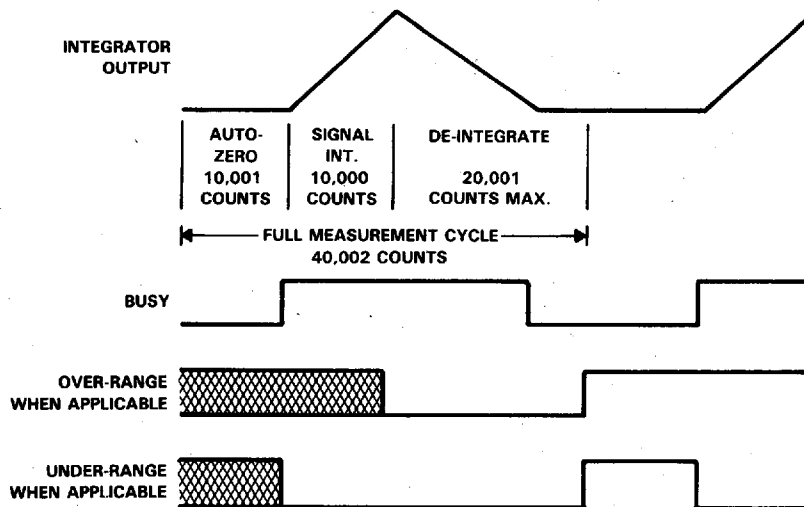
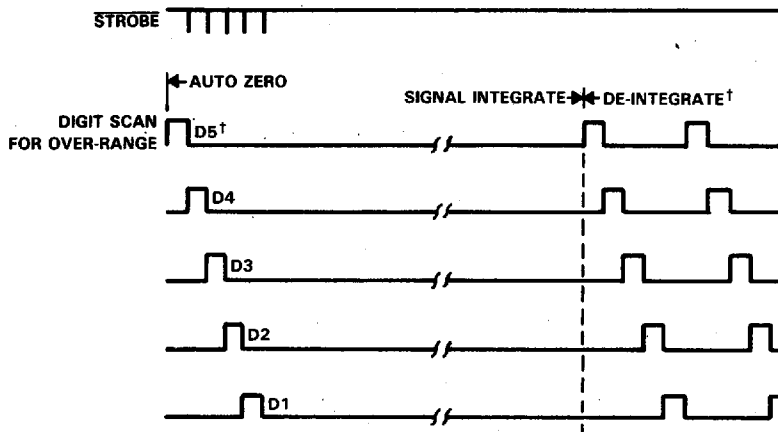


FIGURE 3



†First D5 of AUTO ZERO and DE-INTEGRATE is one count longer.

FIGURE 4

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**ANALOG-TO-DIGITAL CONVERTERS**

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**PRINCIPLES OF OPERATION**

**T-51-10-05**

A measurement cycle for the ICL7135C and TLC7135C consists of the following four phases.

1. **Auto-Zero Phase.** The internal IN+ and IN- inputs are disconnected from the pins and internally connected to ANLG COMMON. The reference capacitor is charged to the reference voltage. The system is configured in a closed loop and the auto-zero capacitor is charged to compensate for offset voltages in the buffer amplifier, integrator, and comparator. The auto-zero accuracy is limited only by the system noise, and the overall offset, as referred to the input, is less than 10  $\mu$ V.
2. **Signal Integrate Phase.** The auto-zero loop is opened and the internal IN+ and IN- inputs are connected to the external pins. The differential voltage between these inputs is integrated for a fixed period of time. If the input signal has no return with respect to the converter power supply, IN- can be tied to ANLG COMMON to establish the correct common-mode voltage. Upon completion of this phase, the polarity of the input signal is recorded.
3. **De-integrate Phase.** The reference is used to perform the de-integrate task. The internal IN- is internally connected to ANLG COMMON and IN+ is connected across the previously charged reference capacitor. The recorded polarity of the input signal is used to ensure that the capacitor will be connected with the correct polarity so that the integrator output polarity will return to zero. The time, which is required for the output to return to zero, is proportional to the amplitude of the input signal. The return time is displayed as a digital reading and is determined by the equation  $10,000 \times (V_{ID}/V_{ref})$ . The maximum or full-scale conversion occurs when  $V_{ID}$  is two times  $V_{ref}$ .
4. **Zero Integrator Phase.** The internal IN- is connected to ANLG COMMON. The system is configured in a closed loop to cause the integrator output to return to zero. Typically this phase requires 100 to 200 clock pulses. However, after an over-range conversion, 6200 pulses are required.

### description of analog circuits

#### input signal range

The common mode range of the input amplifier extends from 1 V above the negative supply to 1 V below the positive supply. Within this range, the common mode rejection ratio (CMRR) is typically 86 dB. Both differential and common mode voltages cause the integrator output to swing. Therefore, care must be exercised to assure the integrator output does not saturate.

#### analog common

Analog common (ANLG COMMON) is connected to the internal IN- during the auto-zero, de-integrate, and zero integrator phases. If IN- is connected to a voltage which is different than analog common during the signal integrate phase, the resulting common mode voltage will be rejected by the amplifier. However, in most applications, IN LO will be set at a known fixed voltage (power supply common for instance). In this application, analog common should be tied to the same point, thus removing the common mode voltage from the converter. Removing the common mode voltage in this manner will slightly increase conversion accuracy.

#### reference

The reference voltage is positive with respect to analog common. The accuracy of the conversion result is dependent upon the quality of the reference. Therefore, to obtain a high accuracy conversion, a high quality reference should be used.

**ICL7135C, TLC7135C**  
**Advanced LinCMOS™ 4 1/2-DIGIT PRECISION**  
**ANALOG-TO-DIGITAL CONVERTERS**

T-51-10-05

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**description of digital circuits****RUN/HOLD input**

When the RUN/HOLD input is high or open, the device will continuously perform measurement cycles every 40,002 clock pulses. If this input is taken low, the IC will continue to perform the ongoing measurement cycle and then hold the conversion reading for as long as the pin is held low. If the pin is held low after completion of a measurement cycle, a short positive pulse (greater than 300 ns) will initiate a new measurement cycle. If this positive pulse occurs before the completion of a measurement cycle, it will not be recognized. The first STROBE pulse, which occurs 101 counts after the end of a measurement cycle, is an indication of the completion of a measurement cycle. Thus, the positive pulse could be used to trigger the start of a new measurement after the first STROBE pulse.

**STROBE input**

Negative going pulses from this input are used to transfer the BCD conversion data to external latches, UARTS, or microprocessors. At the end of the measurement cycle, the digit-drive (D5) input goes high and remains high for 201 counts. The most significant digit (MSD) BCD bits are placed on the BCD pins. After the first 101 counts, halfway through the duration of output D1-D5 going high, the STROBE pin goes low for 1/2 clock pulse width. The placement of the STROBE pulse at the midpoint of the D5 high pulse allows the information to be latched into an external device on either a low-level or an edge. Such placement of the STROBE pulse also ensures that the BCD bits for the second MSD will not yet be competing for the BCD lines and latching of the correct bits is assured. The above process is repeated for the second MSD and the D4 output. Similarly, the process is repeated through the least significant digit (LSD). Subsequently, inputs D5 through D1 and the BCD lines will continue scanning without the inclusion of STROBE pulses. This subsequent continuous scanning causes the conversion results to be continuously displayed. Such subsequent scanning does not occur when an over-range condition occurs.

**BUSY output**

The BUSY output goes high at the beginning of the signal integrate phase and remains high until the first clock pulse after zero-crossing or at the end of the measurement cycle if an over-range condition occurs. It is possible to use the BUSY pin to serially transmit the conversion result. Serial transmission can be accomplished by ANDing the BUSY and CLOCK signals and transmitting the ANDed output. The transmitted output consists of 10,001 clock pulses, which occur during the signal integrate phase, and the number of clock pulses, which occur during the de-integrate phase. The conversion result can be obtained by subtracting 10,001 from the total number of clock pulses.

**OVER-RANGE output**

When an over-range condition occurs, this pin goes high after the BUSY signal goes low at the end of the measurement cycle. As previously noted, the BUSY signal remains high until the end of the measurement cycle when an over-range condition occurs. The OVER-RANGE output goes high at end of BUSY and goes low at the beginning of the de-integrate phase in the next measurement cycle.

**UNDER-RANGE output**

At the end of the BUSY signal, this pin goes high if the conversion result is less than or equal to 9% (count of 1800) of the full-scale range. The UNDER-RANGE output is brought low at the beginning of the signal integrate phase of the next measurement cycle.

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**ICL7135C, TLC7135C**  
**Advanced LinCMOS™ 4 1/2-DIGIT PRECISION**  
**ANALOG-TO-DIGITAL CONVERTERS**

**PRINCIPLES OF OPERATION**

T-51-10-05

**POLARITY output**

The POLARITY output is high for a positive input signal and is updated at the beginning of each de-integrate phase. The polarity output is valid for all inputs including  $\pm 0$  and over-range signals.

**digit-drive (D5, D4, D2 and D1) outputs**

Each digit-drive output (D1 through D5) sequentially goes high for 200 clock pulses. This sequential process is continuous unless an over-range occurs. When an over-range occurs, all of the digit drive outputs are blanked from the end of the strobe sequence until the beginning of the de-integrate phase (when the sequential digit drive activation begins again). The blanking activity, during an over-range condition, may be used to cause the display to flash and indicate the over-range condition.

**BCD outputs**

The BCD bits (B8, B4, B2 and B1) for a given digit are sequentially activated on these outputs. Simultaneously, the appropriate Digit-drive line for the given digit is activated.

**system aspects**

**integrating resistor**

The value of the integrating resistor ( $R_{INT}$ ) is determined by the full scale input voltage and the output current of the integrating amplifier. The integrating amplifier can supply 20  $\mu A$  of current with negligible non-linearity. The equation for determining the value of this resistor is as follows:

$$R_{INT} = \frac{\text{FULL-SCALE VOLTAGE}}{I_{INT}}$$

Integrating amplifier current,  $I_{INT}$ , from 5 to 40  $\mu A$  will yield good results. However, the nominal and recommended current is 20  $\mu A$ .

**integrating capacitor**

The product of the integrating resistor and capacitor should be selected to give the maximum voltage swing without causing the integrating amplifier output to saturate and get too close to the power supply voltages. If the amplifier output is within 0.3 V of either supply, saturation will occur. With  $\pm 5$ -V supplies and ANLG COMMON connected to ground, the designer should design for a  $\pm 3.5$ -V to  $\pm 4$ -V integrating amplifier swing. A nominal capacitor value is 0.47  $\mu F$ . The equation for determining the value of the integrating capacitor ( $C_{INT}$ ) is as follows:

$$C_{INT} = \frac{10,000 \times \text{CLOCK PERIOD} \times I_{INT}}{\text{INTEGRATOR OUTPUT VOLTAGE SWING}}$$

where:  $I_{INT}$  is nominally 20  $\mu A$ .

Capacitors with large tolerances and high dielectric absorption can induce conversion inaccuracies. A capacitor, which is too small could cause the integrating amplifier to saturate. High dielectric absorption causes the effective capacitor value to be different during the signal integrate and de-integrate phases. Polypropylene capacitors have very low dielectric absorption. Polystyrene and Polycarbonate capacitors have higher dielectric absorption, but also work well.

**ICL7135C, TLC7135C****Advanced LinCMOS™ 4 1/2-DIGIT PRECISION  
ANALOG-TO-DIGITAL CONVERTERS**

T-51-10-05

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**PRINCIPLES OF OPERATION****auto-zero and reference capacitor**

Large capacitors will tend to reduce noise in the system. Dielectric absorption is unimportant except during power-up or overload recovery. Typical values are 1  $\mu$ F.

**reference voltage**

For high-accuracy absolute measurements, a high quality reference should be used.

**rollover resistor and diode**

The ICL7135C and TLC7135C have a small rollover error, however it can be corrected. The correction is to connect the cathode of any silicon diode to the INT OUT pin and the anode to a resistor. The other end of the resistor is connected to ANLG COMMON or ground. For the recommended operating conditions the resistor value is 100 k $\Omega$ . This value may be changed to correct any rollover error which has not been corrected. In many non-critical applications, the resistor and diode are not needed.

**maximum clock frequency**

For most dual-slope A/D converters, the maximum conversion rate is limited by the frequency response of the comparator. In this circuit, the comparator follows the integrator ramp with a 3  $\mu$ s delay. Therefore, with a 160-kHz clock frequency (6  $\mu$ s period), half of the first reference integrate clock period is lost in delay. Hence, the meter reading will change from 0 to 1 with a 50- $\mu$ V input, 1 to 2 with a 150- $\mu$ V input, 2 to 3 with a 250- $\mu$ V input, etc. This transition at midpoint is desirable; however, if the clock frequency is increased appreciably above 160 kHz, the instrument will flash "1" on noise peaks even when the input is shorted. The above transition points assume a 2-V input range is equivalent to 20,000 clock cycles.

If the input signal is always of one polarity, comparator delay need not be a limitation. Clock rates of 1 MHz are possible since non-linearity and noise do not increase substantially with frequency. For a fixed clock frequency, the extra count or counts caused by comparator delay will be a constant and can be subtracted out digitally.

For signals with both polarities, the clock frequency can be extended above 160 kHz without error by using a low value resistor in series with the integrating capacitor. This resistor causes the integrator to jump slightly towards the zero-crossing level at the beginning of the de-integrate phase and thus, compensates for the comparator delay. This series resistor should be 10  $\Omega$  to 50  $\Omega$ . This approach allows clock frequencies up to 480 kHz.

**minimum clock frequency**

The minimum clock frequency limitations result from capacitor leakage from the auto-zero and reference capacitors. Measurement cycles as high as 10 s are not influenced by leakage error.

**rejection of 50 Hz or 60 Hz pickup**

To maximize the rejection of 50 Hz or 60 Hz pickup, the clock frequency should be chosen so that an integral multiple of 50 Hz or 60 Hz periods occur during the signal integrate phase. To achieve rejection of these signals, some clock frequencies which could be used are as follows:

50 Hz: 250, 166.66, 125, 100 kHz, etc.

60 Hz: 300, 200, 150, 120, 100, 40, 33.33 kHz, etc.

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**PRINCIPLES OF OPERATION**

T-51-10-05

**zero-crossing flip-flop**

This flip-flop interrogates the comparator's zero-crossing status. The interrogation is performed after the previous clock cycle and the positive half of the ongoing clock cycle have occurred so that any comparator transients which result from the clock pulses do not affect the detection of a zero-crossing. This procedure delays the zero-crossing detection by one clock cycle. To eliminate the inaccuracy, which is caused by this delay, the counter is disabled for one clock cycle at the beginning of the de-integrate phase. Therefore, when the zero-crossing is detected one clock cycle later than the zero-crossing actually occurs, the correct number of counts is displayed.

**noise**

The peak-to-peak noise around zero is approximately 15  $\mu\text{V}$  (peak-to-peak value not exceeded 95% of the time). Near full scale, this value increases to approximately 30  $\mu\text{V}$ . Much of the noise originates in the auto-zero loop, and is proportional to the ratio of the input signal to the reference.

**analog and digital grounds**

For high-accuracy applications, ground loops must be avoided. Return currents from digital circuits must not be sent to the analog ground line.

**power supplies**

The ICL7135C and TLC7135C are designed to work with  $\pm 5\text{-V}$  power supplies. However, 5-V operation is possible if the input signal does not vary more than  $\pm 1.5\text{ V}$  from mid-supply.